# Velocity measurements of dilute suspensions over and through various porous media models

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#### Abstract

This study is focused on the motion of a dilute suspension containing rigid, spherical, non-Brownian, noncolloidal particles flowing over and through porous media models. The flow is confined to very low Reynolds numbers. To examine the velocity distribution particle image velocimetry (PIV) was applied in conjunction with refractive index matching (RIM) techniques. This study is the first of its kind analyzing the interaction between two common engineering systems: suspension fluid and porous media.

### **1** Introduction

Porous media has been a prevalent structure in both the natural world as well as many manufactured systems. Fluid motion over sediment beds Goharzadeh et al. (2005) and coral reefs/ submerged vegetation Ghisalberti and Nepf (2009) have been investigated as natural forms of porous media. Other studies have focused on using optical experimental techniques to investigate the properties at the interface of a porous media bounded on top by a free flow region. Specifically, PIV experiments were developed to identify the effect of the porous media characteristics and different porous media configurations on the overall flow structure and the properties at the interface, Arthur et al. (2009); Agelinchaab et al. (2006). These studies are limited to pure Newtonian fluid over and through porous media.

Much like porous media, suspension flows are observed in natural systems, so they have been commonly utilized in engineering structures. Because of this, optical experimental techniques were developed coupled with RIM techniques to measure the velocity and concentration for suspension flow through various geometries. These PIV experiments have been developed to study various phenomenon within the velocity profile for different types of suspensions, Jesinghausen et al. (2016); Medhi et al. (2011).

By examining previous literature, it was clear that there was a fundamental gap in knowledge that describes how these two systems would interact to one another. These types of systems have been observed in pharmaceuticals, oil mining, and slurry transport. It is important to better understand how the properties of both systems would affect the flow structure. This study using PIV to study how the velocity and interaction properties are effected by the porous media characteristics and the dilute suspension concentration.

The suspension particles were monodispersed polymethyl methacrylate (PMMA) with an average size of 82 $\mu$ m (Cospheric, LLC). The Newtonian solvent was created based off of a solution presented by Lyon and Leal (1998a, 199b) Lyon and Leal (1998a,b). Multiple dimensionless parameters such as particle Reynolds numbers, Stokes number, and Pélect number were all checked to ensure the motion of the suspension particles was solely dependent on the fluid motion. The porous media was made up of rigid rods in a unit square and was created by a 3D printer. This was done so that we could control the various properties of the porous media. There were three dimensionless height parameters,  $\delta = h_p/L$  tested,  $\delta = 4.54, 1.37, 0.74$  and three permeability parameters  $\sigma = L/\sqrt{K}$  tested,  $\sigma = 2.2, 3.46, 6.09$ . In these relationships  $h_p$  is the porous media thickness, *L* is half the free flow height, and *K* is the permeability.



Figure 1: (a) Schematic of the experimental setup, and (b) an image of the experiments in Mirbod's Lab.

#### 2 Results

The velocity fields were extracted from two data collection planes, one plane within the rods of the porous media,  $P_1$ , and one plane placed in the middle on top of the rods,  $P_2$ . These two planes were area averaged together to get the full one-dimensional velocity profile for the flow through the porous media, Arthur et al. (2009). These velocity profiles for the different  $\delta$  values are shown in Fig. 2. In each figure the three different permeability parameters are shown at each constant height ratio. In these figures, as the permeability parameter decreases the lower the velocity profile for the highest permeability parameter. For the other two height ratios there is not much of an effect at  $\sigma = 6.09$ .

Not only are the velocity profiles examined by also the properties at the interface between the free flow region and the top of the porous media. The slip velocity at the interface,  $U_s = |U_{ave}|_{(y/L=0)}$ , Lauga and Stone (2003), is normalized using two different methods. The first is using the maximum velocity in the free flow region, which is shown in Fig. 3(a) for the three different delta values. The other method, known as the dimensionless slip parameter, uses local parameters such as the shear rate  $\dot{\gamma} = |du/dy|_{y=0}$  and the permeability. This parameter better describes the properties at the interface and is known and the dimensionless slip parameter. This is shown in Fig. 2(b) for both data collection planes and the averaged profile. Fig. 3(c) shows the slip length which is length between the actual location of the velocity profile and the location where the parabolic velocity profile would be if it were extrapolated to the interface. Mathematically, this is defined as  $l_{slip} = U_s / |du/dy|_{y=0}$ . Fig.3(a) and Fig.3(c) shows that there is a negative trend as  $\sigma$  increases for all  $\delta$ . Fig. 3(b) shows that as  $\delta$  increases so does the dimensionless slip parameters except for  $\delta = 4.54$  cases which show a negative trend.

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Figure 2: The velocity profiles for various permeability parameters  $\sigma$  and different depth ratio (a)  $\delta = 0.74$ , (b)  $\delta = 1.37$ , and (c)  $\delta = 4.54$ .



Figure 3: (a) The ratio of the slip velocity to the maximum velocity for the various test cases. (b) The dimensionless slip parameter for all test cases and the (d) slip length evaluated at the interface. The error bars were calculated using the velocity uncertainties and methods outlined by Sciacchitano and Wieneke (2016) and Coleman and Steele (1995)

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