

Highly accurate optical flow method based on volumetric segmentation for 3D PIV

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Abstract

In this study, we present a new three-dimensional optical flow method based on volumetric segmentation for the velocity estimation of fluid flow. The proposed method uses a segmented smoothness term that is designed on the assumption that the particle velocity varies continuously in each segmented volume and discontinuously on the surfaces of the segmented volumes. Subsequently, the data term is proposed on the basis of the segmented volumes and the fluid mass conservation equation, which is derived from the Reynolds transport equation. In addition, the robust local level-set method is applied to segment the particle volume according to the velocity distribution of fluid flow. The proposed method is evaluated quantitatively on synthetic data and qualitatively on experimental data, and the velocity results are compared to the advanced 3D velocity estimation methods. The results indicate that the proposed method can obtain velocity fields with greater measurement accuracy for Tomo-PIV.

1 Introduction

As a non-contact velocity measurement technique, particle image velocimetry (PIV) has a very wide range of applications such as aerodynamics, biological fluid mechanics, micro-scale complex flow, etc (Raffel et al., 2018). With the development of laser lighting technology and image acquisition technology, PIV has been extended from 2D velocity measurement to 3D velocity measurement (Lasinger et al., 2020). Tomographic particle image velocimetry (Tomo-PIV), as a 3D three-component velocity measurement technology developed from 2D PIV, has been studied by many researchers (Scarano, 2013). In Tomo-PIV measurement, the tracer particles are first seeded into the fluid flow. Then, a thick laser slice is used to illuminate a measurement volume, which is observed by multiple cameras distributed in different views. Subsequently, the particle distribution in the region of interest is reconstructed by the multiplicative algebraic reconstruction technique (MART) from the multi-view image in each frame (Elsinga et al., 2006). Finally, the 3D velocity field within a chosen interrogation volume is obtained by 3D cross-correlation method (Discetti and Astarita, 2012). Among the various technical problems of Tomo-PIV, improving the accuracy and resolution of the velocity field estimated from the particle volume has received the most attention (Scarano, 2013).

After decades of development, the velocity estimation methods in Tomo-PIV can be divided into cross-correlation-based methods and optical flow-based methods. In 3D cross-correlation methods, the particle volumes are divided into several fixed-size interrogation volumes, the correlation coefficient of two interrogation volumes in two successive particle volumes is calculated through the fast Fourier transform, then the velocity vector in each interrogation volume is determined by the position of the correlation peak (Lu et al., 2021). Because of its strong robustness, the 3D cross-correlation methods have been widely used in Tomo-PIV. Discetti and Astarita (2012) presented a 3D cross-correlation method based on voxel binning for quick estimation of the predicted displacement field. A 3D cross-correlation method based on gradient iterative volume deformation was proposed by Cheminet et al. (2014). Although these 3D cross-correlation methods have achieved significant improvements in accuracy, they still cannot achieve accurate velocity field measurement. The velocity vector obtained by the 3D cross-correlation methods can be interpreted as the spatial average velocity in the interrogation volume. The resolution of the estimated velocity field is restricted by the size of the interrogation volume, which makes it unsuitable for flow field measurement with a rapidly changing velocity field.

Alternatively, the global optical flow method, which can provide velocity fields with pixel-level resolution, has been verified in 2D PIV and extended to Tomo-PIV (Ruhnau et al., 2005). The 3D global optical flow methods use a global energy function composed of a data term and smoothness term to replace the interrogation volume in the 3D cross-correlation methods, in which the data term assumes that the given points retain the same intensity in the particle volume along their trajectories, and the smoothness term assumes that all neighboring points have similar motions. Alvarez et al. (2009) first introduced the global optical flow method to the research field of Tomo-PIV, which includes the incompressibility of the flow as a constraint to the minimization problem. Lasinger et al. (2017) presented a 3D version of the global optical flow model, augmented with a physically based smoothness term for incompressible fluids. Although these 3D global optical flow methods are constantly improving the measurement accuracy of the velocity field in Tomo-PIV, they still cannot obtain results with higher accuracy because of global energy function constraints (Lu et al., 2019). Because the global energy function constraints will make the rapidly changing velocity field too smooth, and the fine structure cannot be preserved. Therefore, improving the accuracy of 3D global optical flow methods for rapidly changing velocity field measurement is an urgent problem to solve.

In this study, we propose a volumetric-segmentation-based optical flow (VS-OF) method for highly accurate Tomo-PIV measurements. A segmented smoothness term is designed on the assumption that the velocity varies continuously within each segmented volume and discontinuously on the surfaces of the segmented volumes. Subsequently, the data term is proposed on the basis of the segmented volumes and the fluid mass conservation equation, which is derived from the Reynolds transport equation. In addition, the robust local level-set method is applied to segment the particle volume according to the velocity distribution of the fluid flow. The rest of the present paper is organized as follows. In section 2, the proposed VS-OF method is described in detail. Experimental analysis is given in section 3. Conclusions drawn from the present work are summarized in section 4.

2 The proposed VS-OF method

2.1 Framework of the VS-OF method

In Tomo-PIV measurement, the accurate measurement of the velocity field is of great significance for the subsequent in-depth analysis of the flow structure. In this study, a volumetric-segmentation-based optical flow method is proposed. The main process of the VS-OF method is shown in Fig. 1. An initial velocity field (u_0, v_0, w_0) is first estimated by the 3D optical flow of the VS-OF method. Subsequently, the initial velocity field is provided as an initialization for the next velocity field segmentation task. According to the segmentation results of the velocity field, the next step of optical flow calculation is guided. After several iterations, the final finer velocity field (u, v, w) is obtained.

In traditional 3D global optical flow methods, due to the global energy function constraints, the velocity field is smoothed in the iterative calculation of optical flow. Therefore, in order to avoid smoothing, the VS-OF method segments the 3D velocity field calculated in the previous step in each optical flow iteration. It should be noted that the segmentation operation is implemented on the three components of the velocity field rather than on the velocity magnitude, as shown in Fig. 1. Then, the particle volumes $E(t)$ and $E(t + dt)$ are segmented according to the segmentation result of the velocity field, and the segmented velocity field is taken as the initial value of the next optical flow iteration. The above process is repeated to obtain an accurate 3D velocity field. The proposed VS-OF method has excellent comprehensive performance in terms of flow velocity estimation due to the process of velocity field segmentation. The segmented smoothness term and data term in the VS-OF method will be presented and discussed in the following subsections.

2.2 A segmented smoothness term

Inspired by the level set segmentation method (Li et al., 2007), a segmented smoothness term is designed on the assumption that the velocity varies continuously within each segmented volume and discontinuously on the surfaces of the segmented volumes. In addition, the segmented smoothness term can segment the particle volume according to the 3D velocity distribution of the fluid flow. Without loss of generality, we simplify the smoothness term to consider only the u component—that is, to minimize Eq. 1:

$$\int_{\Omega_u} K_\sigma |\nabla u|^2 dx + \int_{\Omega_u^c} K_\sigma |\nabla u|^2 dx + \mu |S_u| \quad (1)$$

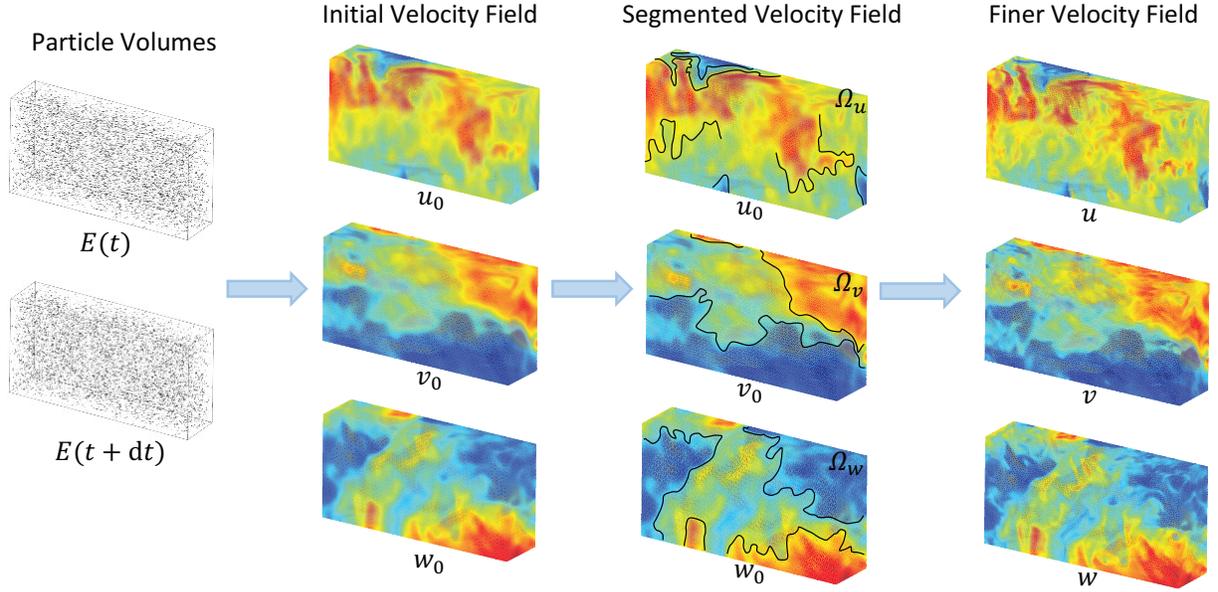


Figure 1: Concept of the proposed VS-OF method.

where $\mathbf{u} = (u, v, w)^T$ is the velocity vector at location \mathbf{x} , Ω_u denotes the segmented volumes in the u component, Ω_u^C is the complement of Ω_u , S_u is the closed parameterized surface of the segmented volumes Ω_u , $|S_u|$ is the area of surface S_u , μ is a parameter constraining the surface of a segmented volume to be as smooth as possible, and K_σ denotes a Gaussian kernel with standard deviation σ .

Drawing lessons from the idea of (Li et al., 2007), the unknown evolution surface is replaced with the level set function $\Phi_u(\mathbf{x})$: $\Phi_u(\mathbf{x}) > 0$ if \mathbf{x} is inside the closed surface S_u , $\Phi_u(\mathbf{x}) < 0$ if \mathbf{x} is outside S_u , and $\Phi_u(\mathbf{x}) = 0$ if \mathbf{x} is on S_u . We can approximate $|S_u| = \int_\Omega |\nabla H(\Phi_u)| d\mathbf{x} = \int_\Omega \delta(\Phi_u) |\nabla \Phi_u| d\mathbf{x}$, and Eq. 1 can be rewritten as follows:

$$\begin{aligned} & \int_\Omega \left(H(\Phi_u) K_\sigma |\nabla u|^2 + (1 - H(\Phi_u)) K_\sigma |\nabla u|^2 \right) d\mathbf{x} + \int_\Omega \mu \delta(\Phi_u) |\nabla \Phi_u| d\mathbf{x} \\ &= \int_\Omega \left(K_\sigma |\nabla u|^2 + \mu \delta(\Phi_u) |\nabla \Phi_u| \right) d\mathbf{x} \end{aligned} \quad (2)$$

where $H(\Phi)$ is the Heaviside function, which is equal to 1 if $\Phi \geq 0$ and to 0 if $\Phi < 0$; $\delta(\Phi)$ is the Dirac function, and $\delta(\Phi) = H'(\Phi)$. Generally, the Heaviside function $H(\Phi)$ in Eq. 2 is approximated by a smooth function defined by:

$$H(\Phi) = \frac{1}{2} \left[1 + \frac{2}{\pi} \arctan(\Phi) \right] \quad (3)$$

The Dirac function $\delta(\Phi)$, the derivative of $H(\Phi)$, is the following smooth function:

$$\delta(\Phi) = H'(\Phi) = \frac{1}{\pi} \frac{1}{1 + \Phi^2} \quad (4)$$

We now extend the segmented smoothness term to three components, and Eq. 2 can be expressed as follows:

$$\begin{aligned} E_{smooth}^{VS} &= \int_\Omega \left(K_\sigma |\nabla u|^2 + \mu \delta(\Phi_u) |\nabla \Phi_u| \right) d\mathbf{x} + \int_\Omega \left(K_\sigma |\nabla v|^2 + \mu \delta(\Phi_v) |\nabla \Phi_v| \right) d\mathbf{x} \\ &+ \int_\Omega \left(K_\sigma |\nabla w|^2 + \mu \delta(\Phi_w) |\nabla \Phi_w| \right) d\mathbf{x} \end{aligned} \quad (5)$$

2.3 A segmented data term

Define a new segmentation surface S_0 based on the segmented surface S_u , S_v and S_w : $S_0 = S_u \cup S_v \cup S_w = \{(x, y, z) | \Phi_u(x, y, z) = 0, \Phi_v(x, y, z) = 0, \Phi_w(x, y, z) = 0\}$, and Ω_0 denotes the segmented volume surrounded by S_0 . Consistent with the smoothness term, we replace the segmented surface S_0 with the level set function Φ_0 . Therefore, we propose the segmented data term on the basis of the fluid mass conservation equation, which is derived from the Reynolds transport equation:

$$\int_{\Omega_0} \left(\frac{\partial E}{\partial t} + \nabla E \cdot \mathbf{u} + E \operatorname{div} \mathbf{u} \right)^2 \mathrm{d}\mathbf{x} + \int_{\Omega_0^c} \left(\frac{\partial E}{\partial t} + \nabla E \cdot \mathbf{u} + E \operatorname{div} \mathbf{u} \right)^2 \mathrm{d}\mathbf{x} \quad (6)$$

In addition, for the segmented volumes, the material density in the fluid remains constant, and the divergence of the velocity is zero: $\operatorname{div} \mathbf{u} = \nabla \cdot \mathbf{u} = 0$. In other words, the fluid is incompressible in each segmented volume Ω_0 . We can derive a simplified segmented data term by constraining $\operatorname{div} \mathbf{u} = 0$:

$$\begin{aligned} E_{data}^{VS} &= \int_{\Omega} H(\Phi_0) \left(\frac{\partial E}{\partial t} + \nabla E \cdot \mathbf{u} \right)^2 \mathrm{d}\mathbf{x} + \int_{\Omega} (1 - H(\Phi_0)) \left(\frac{\partial E}{\partial t} + \nabla E \cdot \mathbf{u} \right)^2 \mathrm{d}\mathbf{x} \\ &= \int_{\Omega} \left(\frac{\partial E}{\partial t} + \nabla E \cdot \mathbf{u} \right)^2 \mathrm{d}\mathbf{x} \end{aligned} \quad (7)$$

where Ω is the entire particle volume. Based on Eqs. 5 and 7, the model of the proposed VS-OF method is as follows:

$$\begin{aligned} E^{VS} &= \alpha E_{data}^{VS} + E_{smooth}^{VS} \\ &= \alpha \int_{\Omega} \left(\frac{\partial E}{\partial t} + \nabla E \cdot \mathbf{u} \right)^2 \mathrm{d}\mathbf{x} + \int_{\Omega} \left(K_{\sigma} |\nabla u|^2 + \mu \delta(\Phi_u) |\nabla \Phi_u| \right) \mathrm{d}\mathbf{x} \\ &\quad + \int_{\Omega} \left(K_{\sigma} |\nabla v|^2 + \mu \delta(\Phi_v) |\nabla \Phi_v| \right) \mathrm{d}\mathbf{x} + \int_{\Omega} \left(K_{\sigma} |\nabla w|^2 + \mu \delta(\Phi_w) |\nabla \Phi_w| \right) \mathrm{d}\mathbf{x} \end{aligned} \quad (8)$$

where α is a parameter controlling the balance between the data term and smoothness term. Finally, the multiscale technique and image warping operation are implemented in the segmented particle volumes to avoid falling into local optimal solutions and obtain an accurate velocity field.

3 Experimental analysis

3.1 Experimental setup

In order to make a quantitative comparison with the proposed VS-OF method, we extend the multiple-pass cross-correlation method provided by Thielicke and Stamhuis (2014) and the global optical flow method proposed by Ruhnau et al. (2005) to three dimensions. In terms of numerical evaluation indicators, the root mean square error (RMSE) and average angle error (AAE), which are often used to verify accuracy in the field of optical flow (Alvarez et al., 2009; Lu et al., 2019), are used to quantitatively evaluate the experimental results:

$$\operatorname{RMSE} = \sqrt{\frac{1}{N} \sum_{i=1}^N |\mathbf{u}_i^t - \mathbf{u}_i^e|^2} \quad (9)$$

$$\operatorname{AAE} = \frac{1}{N} \sum_{i=1}^N \arccos \left(\frac{\mathbf{u}_i^t \cdot \mathbf{u}_i^e}{|\mathbf{u}_i^t| |\mathbf{u}_i^e|} \right) \quad (10)$$

where \mathbf{u}^t and \mathbf{u}^e denote the ground truth and the estimated velocity field, respectively. N is the total number of voxels in the estimated particle volume, and the subscript i represents the voxel coordinates.

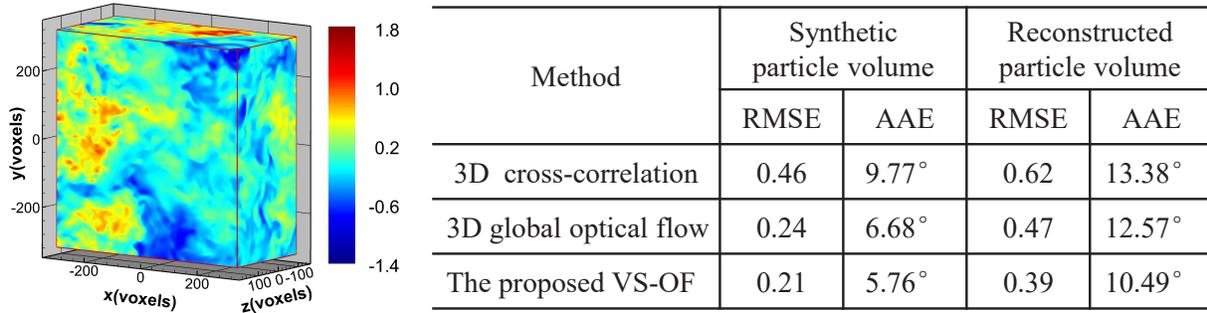


Figure 2: Left: Velocity contours of the ground truth in the u component. Right: RMSE and AAE errors of the velocity fields for the synthetic and reconstructed particle volumes estimated by different methods.

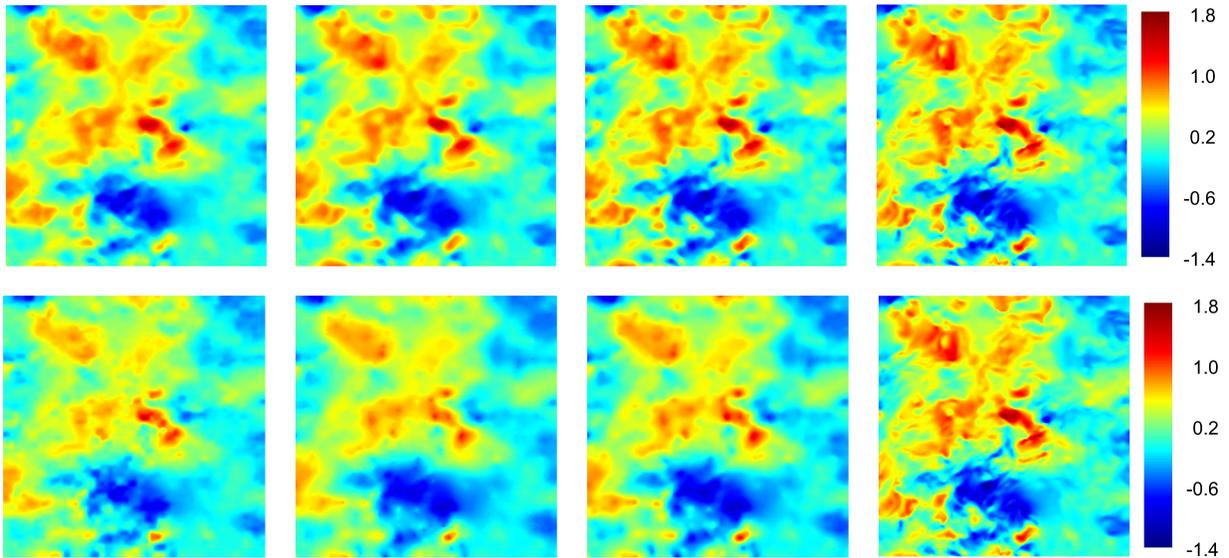


Figure 3: Velocity contours estimated from the synthetic particle volumes (top) and reconstructed particle volumes (bottom) in the u component on the $z = 0$ plane. Left to right: Contours estimated by the 3D cross-correlation method, the 3D global optical flow method, and the proposed VS-OF method, as well as the ground truth.

3.2 Synthetic data

In the synthetic data, the ground truth velocity field from the Johns Hopkins Turbulence Database provided by Li et al. (2008) is used to quantitatively evaluate the proposed VS-OF method. The velocity field comprises a numerically generated 3D isotropic turbulent flow with an average velocity of 1.3 voxels and a maximum velocity of 2.9 voxels. A synthetic particle volume of $640 \times 640 \times 300$ voxels is generated with a random seed density of approximately 0.1 particles per pixel. The particles are projected onto four cameras with 1024×1024 pixels at viewing angles of $\pm 35^\circ$ with respect to the $x = 0$ plane and $\pm 18^\circ$ with respect to the $y = 0$ plane. Then, the particle volume is reconstructed using the reimplementation of MART proposed by Scarano (2013) with a quality factor $Q = 0.79$.

To distinguish the influence of MART, the synthetic particle volume (without MART) and the reconstructed particle volume (with MART) are used to evaluate the different methods. The results for the synthetic and reconstructed particle volumes estimated by the different methods are presented in Fig. 2. Due to the influence of MART, the RMSE and AAE errors of the reconstructed particle volume are larger than those of the synthetic particle volume, but the errors of the proposed VS-OF method are smaller than those of the other two methods on both the synthetic and the reconstructed particle volumes. The velocity contours in the u component on the $z = 0$ plane estimated by the proposed VS-OF method exhibit behavior similar to the ground truth, as shown in Fig. 3.

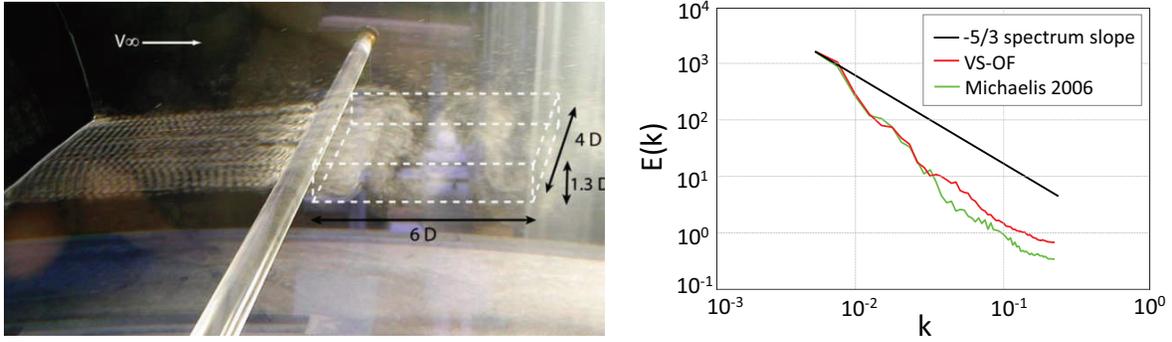


Figure 4: Left: Real experiment scene of cylinder wake (Michaelis et al., 2006). Right: Spectrum analysis of the velocity fields for the experimental data.

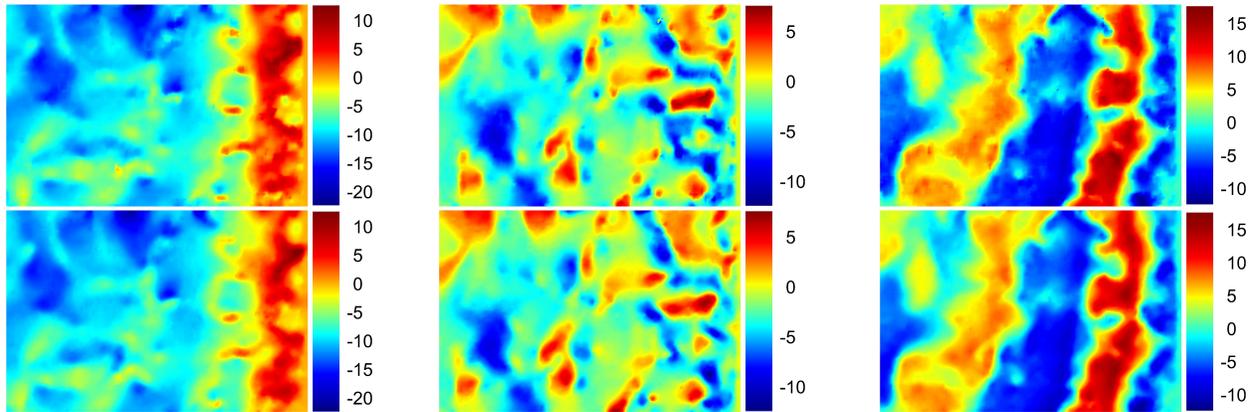


Figure 5: Velocity contours in the xy -slice of the flow on the $z = 203$ plane. Top to bottom: Reference flow field in u , v , and w components provided by Michaelis et al. (2006); estimated flow field in u , v , and w components by the proposed VS-OF method.

3.3 Experimental data

In this subsection, we present qualitative results of the experimental data in the water flow (Michaelis et al., 2006). The experimental data package contains of two particle volumes of $2107 \times 1434 \times 406$ voxels. It is a Karman vortex street behind a cylinder with a diameter $D = 12\text{mm}$, which is positioned to the left of the volume, with water flowing to the right, as shown in Fig. 4.

The velocity contours in the xy -slice of the flow on the $z = 203$ plane estimated by the proposed VS-OF method are shown in Fig. 5. In addition to our own results, we also show the reference flow field provided in the experimental data package, which is processed by the 3D cross-correlation method (Elsinga et al., 2006). The results indicate that our method can better preserve the flow field structure with a rapidly changing velocity field compared to the reference flow. To better investigate the performance of the proposed VS-OF method, spectrum analysis is performed for the two processing methods, as shown in Fig. 4. The spectrum obtained by the proposed VS-OF method is closer to the $-5/3$ spectrum slope. From this experiment, we can conclude that the proposed VS-OF method is suitable for velocity field estimation in experimental data.

4 Conclusions

In this study, we propose a novel 3D optical flow method based on volumetric segmentation for the velocity estimation of fluid flow. The proposed VS-OF method uses a segmented smoothness term designed on the assumption that the particle velocity varies continuously in each segmented volume and discontinuously on the surfaces of the segmented volumes. The data term is proposed on the basis of the segmented volumes and the fluid mass conservation equation, which is derived from the Reynolds transport equation. In addition, the

robust local level-set method is applied to segment the particle volume according to the velocity distribution of the fluid flow. To verify the performance of the proposed VS-OF method, we evaluate it quantitatively on synthetic data and qualitatively on experimental data. It can be seen from the synthetic data that compared with the 3D cross-correlation method and 3D global optical flow method, the proposed VS-OF method can obtain velocity fields with greater accuracy. Finally, we demonstrate the good performance of the proposed VS-OF method in a real cylinder wake flow experiment.

Acknowledgements

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